

Na bazi premera dela sastojine crnog bora u Lipovici, površine $p = 0.1$ ha i poznate starosti od 55 godina, odrediti i analizirati sledeće elemente rasta i sastojinske izgrađenosti i po potrebi ih grafički predstaviti:

1. Srednje prečnike i visine; 2. Temeljnice i zapremine;

2.1. Temeljnice pojedinačnih stabla, dobijene izrazom $g = \frac{d^2 \cdot \pi}{40000}$, upisivati u tabelu koja je u sklopu ovog zadatka.

2.2. Na osnovu stepene funkcije, $h = 7.6534407 \cdot d^{0.2943235}$, pomoću koja smo izravnavali vezu prečnika i visine nacrtati visinsku krivu na grafikonu iz prethodnog zadatka. Takođe, na osnovu dobijene visinske krive, odrediti i upisati visine na mestima gde nedostaju u tabeli premera iz prethodnog zadatka.

–	d [cm]	+	v [m^3]
9.5	10	10.49	$0.003321 + 0.0019551 \cdot h + 0.000212 \cdot h^2 - 0.000008449883 \cdot h^3$
10.5	11	11.49	$0.019433 - 0.00197 \cdot h + 0.000608 \cdot h^2 - 0.000018 \cdot h^3$
11.5	12	12.49	$-0.032979 + 0.013841 \cdot h - 0.000671 \cdot h^2 + 0.000015 \cdot h^3$
12.5	13	13.49	$-0.018609 + 0.012202 \cdot h - 0.000566 \cdot h^2 + 0.000015 \cdot h^3$
13.5	14	14.49	$-0.044235 + 0.019489 \cdot h - 0.001044 \cdot h^2 + 0.000026 \cdot h^3$
14.5	15	15.49	$-0.019722 + 0.014333 \cdot h - 0.000514 \cdot h^2 + 0.000012 \cdot h^3$
15.5	16	16.49	$-0.007571 + 0.012104 \cdot h - 0.000137 \cdot h^2$
16.5	17	17.49	$0.01 + 0.01 \cdot h$
17.5	18	18.49	$0.223156 - 0.059532 \cdot h + 0.008337 \cdot h^2 - 0.000414 \cdot h^3 + 0.000007327232 \cdot h^4$
18.5	19	19.49	$0.013912 + 0.012462 \cdot h$
19.5	20	20.49	$0.017538 + 0.01378 \cdot h$
20.5	21	21.49	$-0.044633 + 0.031277 \cdot h - 0.001271 \cdot h^2 + 0.000032 \cdot h^3$
21.5	22	22.49	$0.023077 + 0.016703 \cdot h$
22.5	23	23.49	$0.026154 + 0.018297 \cdot h$
23.5	24	24.49	$0.03 + 0.02 \cdot h$
24.5	25	25.49	$0.0338462 + 0.0213187 \cdot h$
25.5	26	26.49	$0.042582 + 0.022802 \cdot h$
26.5	27	27.49	$-0.110769 + 0.057962 \cdot h - 0.002315 \cdot h^2 + 0.000052 \cdot h^3$
27.5	28	28.49	$-0.010869 + 0.038017 \cdot h - 0.000767 \cdot h^2 + 0.000017 \cdot h^3$
28.5	29	29.49	$0.232198 - 0.012326 \cdot h + 0.002885 \cdot h^2 - 0.000064 \cdot h^3$
29.5	30	30.49	$0.156749 + 0.00896 \cdot h + 0.001426 \cdot h^2 - 0.000029 \cdot h^3$
30.5	31	31.49	$0.088979 + 0.024003 \cdot h + 0.000711 \cdot h^2 - 0.000018 \cdot h^3$
31.5	32	32.49	$0.025502 + 0.036402 \cdot h + 0.000158 \cdot h^2 - 0.000007331993 \cdot h^3$
32.5	33	33.49	$-0.046558 + 0.051162 \cdot h - 0.000499 \cdot h^2 + 0.000003351768 \cdot h^3$
33.5	34	34.49	$-0.149239 + 0.07371 \cdot h - 0.001758 \cdot h^2 + 0.000029 \cdot h^3$
34.5	35	35.49	$-0.148236 + 0.077322 \cdot h - 0.001863 \cdot h^2 + 0.000031 \cdot h^3$
35.5	36	36.49	$-0.084291 + 0.07077 \cdot h - 0.001462 \cdot h^2 + 0.000025 \cdot h^3$
36.5	37	37.49	$-0.124446 + 0.081256 \cdot h - 0.001933 \cdot h^2 + 0.000034 \cdot h^3$
37.5	38	38.49	$-0.232142 + 0.103519 \cdot h - 0.003053 \cdot h^2 + 0.000055 \cdot h^3$
38.5	39	39.49	$-0.029622 + 0.074514 \cdot h - 0.001407 \cdot h^2 + 0.000026 \cdot h^3$

Za određivanje zapremine po jednosantimetarskim debljinskim stepenima, prvo treba locirati kojem stepenu pripada stablo za koje sve vrši izračunavanje, a zatim u pripadajuću regresionu jednačinu zameniti nezavisnu promenljivu iznosom visine (h) u metrima.

2.3. Trenutni broj stabala iznosi $N/ha = n \cdot \frac{1ha}{p} =$

2.4. Trenutna temeljnica sastojine iznosi $G = \sum_1^n g \cdot \frac{1ha}{p} =$

2.5. Trenutna zapremina sastojine iznosi $V = \sum_1^n v \cdot \frac{1ha}{p} =$

n	g	v	$\frac{h}{d}$	r_s	b	l	$\frac{l}{h}$	$\frac{b}{h}$	$\frac{b}{l}$	$\frac{b}{d}$	Zp	N	G	V	n	g	v	$\frac{h}{d}$	r_s	b	l	$\frac{l}{h}$	$\frac{b}{h}$	$\frac{b}{l}$	$\frac{b}{d}$	Zp	N	G	V	
1	0.05	0.5													45	0.03	0.31													
2	0.05	.													46	.	0.5		2	4			.			15.3	12.6	675	33.8	.
3	.	0.38		.	3.8			.		16.7	.	752	.	285.8	47	0.05	0.46	71	1.8	.	5.3	0.3	0.2	.	14.1	10.2	833	41.7	383.2	
4	0.03	0.21													48	.	0.6	.	.	.	.	.	0.2	.	15.7	.	512	.	307.2	
5	0.06	0.59		2.2	.			0.2		.	.	.	.	329.8	49	0.04	0.33	80			.	0.2								
6	0.08	0.87	72	.	4.6			.		.	.	.	41	.	50	/														
7	.	0.58	63												51	0.04	0.38													
8	0.04	.													52	0.03	0.24													
9	0.03	0.24													53	0.03	0.24													
10	0.03	0.21													54	0.02	0.21													
11	0.04	0.38													55	0.04	0.38													
12	0.04	.													56	/														
13	0.04	0.34													57	0.05	0.46													
14	0.06	0.59													58	0.07	0.68	66	2.7	.	5.8	0.3	0.3	0.9	.	22.9	371	26	.	
15	0.07	0.64	64	2.3	4.6	5.1	.	0.2	.	15.4	16.6	.	35.8	.	59	0.05	0.5		1.9	.			0.2		14.8	11.3	.	37.6	.	
16	.	0.27													60	0.07	0.77	.	.	.	7.4	0.3	.	.	.	.	.	32.9	361.9	
17	0.07	0.73	68	2.1	4.2			0.2		13.7	.	.	42.8	446.8	61	0.05	0.48	85	2	4	7.9	0.4	0.2	.	16.1	12.6	675	33.8	324	
18	.	0.51	.	.	3.6	.	0.3	0.2	.	13.3	10.2	833	50	424.8	62	0.04	0.31		3.4				0.2		16	9.1	.	.	289.5	
19	0.02	0.19	106			3.7	.								63	0.06	0.67	76	.	.	7.5	.	0.2	.	14.6	13.9	612	.	.	
20	0.05	0.42		1.8	3.6			0.2		14.8	.	833	41.7	349.9	64	0.03	.													
21	0.04	0.38													65	0.05	0.54	.			7.2	0.3								
22	0.04	.													66	0.08	0.79	74	2.5	5	7.6	0.3	0.2	.	16.1	19.6	434	34.7	.	
23	0.06	0.59		2	.			0.2		14.4	.	675	40.5	.	67	0.06	0.55	75	2.2	.	.	0.4	0.2	.	16.3	15.2	559	33.5	307.5	
24	0.02	0.16													68	0.05	0.52	80			6.4	0.3								
25	0.03	0.27													69	.	.	.			.	.								
26	0.01	0.09													70	0.04	0.35	90			.	.								
27	0.03	0.27													71	0.03	0.29	87			.	.								
28	0.09	.	69	2.6	5.2			0.2		.	.	.	36.1	360.9	72	0.05	0.42	79	2.1	4.2	.	0.3	.	.	.	13.9	.	30.6	257	
29	0.04	0.34													73	/														
30	0.11	1.18	65												74	0.04	0.4	.			6.1	0.3								
31	0.05	0.49	87			7	.								75	0.06	0.51	63												
32	0.05	.	91			.	0.3								76	0.1	1.1	65												
33	0.07	0.71	71			6	0.3								77	0.05	0.5													
34	0.01	0.08	.			3.1	0.2								78	/														
35	0.04	.													79	.	0.5													
36	0.05	0.42													80	0.02	0.19													
37	0.06	0.59													81	0.08	0.85	.	.	5.8			.		.	26.4	322	.	273.7	
38	/														82	0.04	0.42													
39	0.03	0.22	.			3.7	.								83	0.04	0.34													
40	.	0.54		.	.			0.2		17	16.6	512	30.7	276.5	84	0.04	0.38													
41	0.05	0.45		2	4			0.2		16.3	12.6	675	.	303.8	85	.	.	65	2.5	5			.		.	19.6	.	30.4	260.4	
42	0.05	0.5		2.3	4.6			.		17.8	.	512	.	.	86	0.03	0.28	94			.	.								
43	0.06	0.52	.	2.4	4.8			.		18.1	470	.	244.4	87	0.04	0.42		1.9	3.8			.		.	11.3	752	.	315.8		
44	0.05	0.45		.	4.2			0.2		16.9	13.9	612	30.6	.																